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Chiral structures and defects of lyotropic chromonic liquid crystals induced by saddle-splay elasticity

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An experimental and theoretical study of lyotropic chromonic liquid crystals (LCLCs) confined in cylinders with degenerate planar boundary conditions elucidates LCLC director configurations. When the Frank saddle-splay modulus is more than twice the twist modulus, the ground state adopts an inhomogeneous escaped-twisted configuration. Analysis of the configuration yields a large saddle-splay modulus, which violates Ericksen inequalities but not thermodynamic stability. Lastly, we observe point defects between opposite-handed domains, and we explain a preference for point defects over domain walls.

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The elastic properties of nematic liquid crystals (LCs) are crucial for liquid crystal display applications [1,2], and they continue to give rise to unanticipated fundamental phenomena [3–9]. Three of the bulk nematic LC deformation modes—splay, twist, and bend—are well known and have associated elastic moduli K_1 , K_2 , and K_3 , respectively. These moduli have been studied intensely because they are easy to visualize, and because it is possible to independently excite the modes via clever usage of sample geometry [10–12], LC boundary conditions [13,14], and external fields [15,16]. As a result, these moduli have been measured for a variety of thermotropic and lyotropic LCs [12,16–20]. By contrast, a much less studied fourth independent mode [21–23] of elastic deformation in nematic LCs can exist; it is called saddle-splay. Saddle-splay is hard to visualize and to independently excite [23,24]. Moreover, the energy of this deformation class can be integrated to the boundary, so that the mode does not appear in the Euler-Lagrange equations, and with fixed boundary conditions the saddle-splay energy will have no effect on the LC director configuration. Even with free boundary conditions, the saddle-splay energy will not affect the bulk LC configuration unless the principal curvatures of the surface are different, i.e., saddle-splay effects are not expected for spherical or flat surfaces. Thus, although much progress in understanding saddle-splay has been made [25,26], especially with thermotropic nematic LCs, unambiguous determination of saddle-splay energy effects on liquid crystal configurations and measurement of the saddle-splay elastic modulus, K_{24} , remain difficult [27].

While the bulk elastic constants described above strongly influence LC director configurations, LC boundary conditions at material interfaces also influence bulk structure. Indeed, considerable effort has gone into development of surface preparation techniques to produce particular bulk director configurations [13,28–33]. The saddle-splay term integrates to the boundary and effectively imposes boundary conditions at free surfaces favoring director alignment along the direction of highest surface curvature for positive K_{24} [34] and outwardly

pointing surface normals. For this effect to be present, the director cannot be held perpendicular to the surface, as was the case in our prior work [4]. The potential role of saddle-splay effects in determining bulk director configurations by spontaneous symmetry breaking has been appreciated [13,35–37] but has been difficult to fully characterize; generally, molecular surface forces can impose preferred boundary conditions that are hard to disentangle from effects due to K_{24} [38,39]. As a result, the measurements of K_{24} to date have wide confidence intervals [36,40,41] and even vary in sign [41]. Finally, additional factors that have complicated assignment of saddle-splay effects are the so-called Ericksen inequalities [42] that require $0 < K_{24} < 2K_2$ and $K_{24} < 2K_1$. These inequalities were derived assuming spatially uniform gradients of the director. They do not, however, apply in geometries such as ours, in which gradients are not uniform.

In this paper, we investigate director configurations of the nematic lyotropic chromonic liquid crystal (LCLC) Sunset Yellow (SSY) confined within cylindrical glass capillaries with degenerate planar boundary conditions as initially reported in Refs. [43–45]. Our study employs a combination of polarized optical microscopy, measurements of director-field thermal fluctuations, and Frank-free-energy calculations to rationalize the observed structures. Importantly, we show that a large K_{24} leads to an escaped-twist (ET) ground state, which exhibits a classic double-twist configuration. Note that chiral symmetry breaking in the ET configuration is fundamentally different from symmetry breaking in other LCLC systems with uniform principal curvatures [3], or with homeotropic boundary conditions [4]. In previous work, spontaneous twist deformation arose because K_2 is much smaller than K_1 and K_3 ; K_{24} played no role in the energetics. In the present work, comparison of theory and experiment enables us to measure K_{24} in a LCLC; we find a value of $K_{24}/K_2 = 55.0$, which strongly violates the Ericksen inequalities. Finally, we observe and characterize chiral hedgehog point defects separating chiral domains of opposite handedness. Interestingly, the presence of point defects rather than smooth domain walls also provides precise quantitative information about K_{24} that is consistent with our other conclusions.

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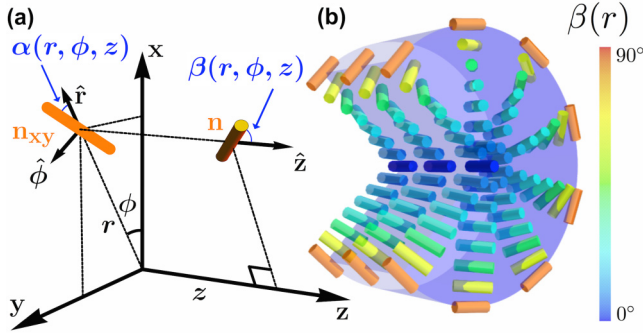


FIG. 1. (Color online) (a) Coordinate system used for director configuration and defect energy calculations. The director \mathbf{n} is described by the angle α between the director projection \mathbf{n}_{xy} and $\hat{\mathbf{r}}$, and by the angle β between \mathbf{n} and the capillary axis, which is parallel to $\hat{\mathbf{z}}$. (b) 3D cutaway view of the capillary and the ground-state director field using $K_2/K_3 = 0.1$ and $K_{24}/K_3 = 4.6$, which approximates the Frank moduli of 30% wt./wt. SSY at 25 °C. Notice the large twist angle at the capillary surface close to 90°. α is independent of position and β depends only on the radial coordinate r . This configuration has right-handed chirality.

Before discussing the experimental results, we formulate the theoretical problem. We assume the achiral nematic LCLC is described by a Frank free energy, i.e.,

$$F = \int d^3\mathbf{x} \left[\frac{1}{2} K_1 (\mathbf{n} \cdot \nabla \cdot \mathbf{n})^2 + \frac{1}{2} K_2 (\mathbf{n} \cdot \nabla \times \mathbf{n})^2 + \frac{1}{2} K_3 (\mathbf{n} \times \nabla \times \mathbf{n})^2 - \frac{1}{2} K_{24} \nabla \cdot (\mathbf{n} \times \nabla \times \mathbf{n} + \mathbf{n} \nabla \cdot \mathbf{n}) \right], \quad (1)$$

where \mathbf{n} is the nematic director. Equation (1) explicitly includes the saddle-splay term with modulus K_{24} , which can in principle be mimicked by a surface anchoring term that is coupled to surface curvature; thus we consider a saddle-splay term that combines the two effects [46–48]. A Rapini-Papoular-type surface anchoring term with in-plane anisotropy [22,38] is excluded and discussed later in the text. The LC is contained inside a capillary of radius R , and cylindrical coordinates are used to parametrize its director field, \mathbf{n} , with $\hat{\mathbf{z}}$ along the capillary axis (see Fig. 1), i.e.,

$$\mathbf{n} = \cos \alpha \sin \beta \hat{\mathbf{r}} + \sin \alpha \sin \beta \hat{\boldsymbol{\phi}} + \cos \beta \hat{\mathbf{z}}. \quad (2)$$

To determine the configuration of the ground state, we assume the director depends only on r , and we minimize the Frank free energy with respect to $\alpha(r)$ and $\beta(r)$. Degenerate planar anchoring conditions at the capillary surface prevent the director from having an $\hat{\mathbf{r}}$ component, so $\alpha(r = R) = \pi/2$. Cylindrical symmetry sets $\beta(r = 0) = 0$. Both $\alpha(r = 0)$ and $\beta(r = R)$ are free to vary, but stationarity of the free energy provides the boundary conditions: $\partial_r \alpha(r = 0) = 0$ and $R \partial_r \beta(r = R) = (\frac{K_{24}}{2K_3} - \frac{1}{2}) \sin 2\beta(r = R)$.

With these boundary conditions, the Euler-Lagrange equations of the Frank free energy give [38]

$$\alpha(r) = \frac{\pi}{2}, \quad (3)$$

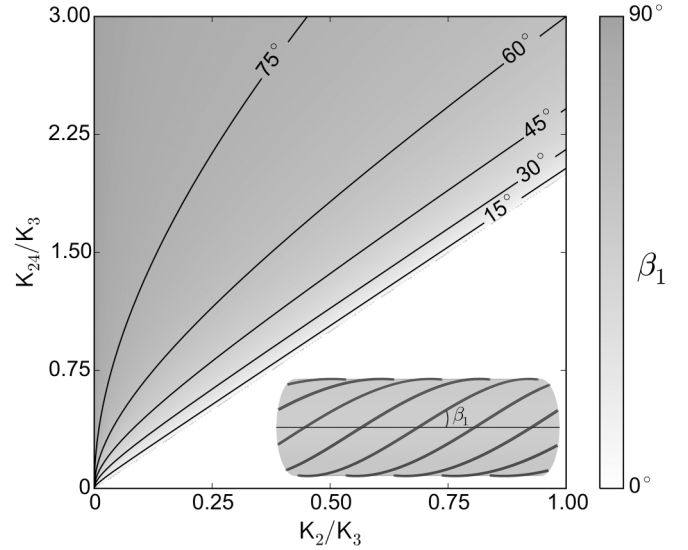


FIG. 2. Phase diagram of β_1 , the angle between the nematic director and the capillary axis at the capillary surface, as a function of elastic moduli ratios of saddle splay (K_{24}) to twist (K_2) and bend (K_3). Inset: an example capillary with streamlines indicating a surface director field at angle β_1 with left-handed chirality.

$$\beta(r) = \arctan \frac{2\sqrt{K_2 K_{24} (K_{24} - 2K_2)} r / R}{\sqrt{K_3} [K_{24} - (K_{24} - 2K_2) r^2 / R^2]}. \quad (4)$$

This ET solution exists for $K_{24} > 2K_2$ and has right-handed chirality, i.e., the director streamlines form right-handed helices. A mirror-image solution $\beta(r) \rightarrow \pi - \beta(r)$ exists with the same energy. Notice that the radial position r is scaled by the cylinder radius R , and that K_1 does not appear because this configuration has no splay. If $K_{24} < 2K_2$, then only the trivial $\beta(r) = 0$ solution exists, which corresponds to the simple parallel-axial configuration [35]. As K_{24} surpasses $2K_2 \equiv K_c$, which is exactly the upper bound found by Ericksen, the system spontaneously breaks chiral symmetry, and an ET configuration of one-handedness grows continuously from the trivial solution. $\beta_1 = \beta(r = R)$ is plotted in Fig. 2. Prior work with thermotropic LCs found this ET configuration when an azimuthal anchoring condition dominates the behavior of β_1 at the capillary surface through a chemical or mechanical treatment of the surface [38,39,49]. $\beta(r)$ [Eq. (4)] can only be approximated by a linear twist model [34] for certain ratios of elastic constants. For LCs whose elastic moduli do not satisfy these ratios, such as SSY, polarized optical microscopy textures are strongly affected by the nonlinear behavior of $\beta(r)$ [47].

The normalized free energy of the ET configuration is readily calculated to be

$$\frac{F}{\pi L} = -(K_{24} - 2K_2) + \frac{\sqrt{K_2 K_3}}{\sqrt{K_3 - K_2}} \arctan \frac{\sqrt{K_3 - K_2} (K_{24} - 2K_2)}{\sqrt{K_2} (K_3 + K_{24} - 2K_2)}, \quad (5)$$

where L is the length of the capillary. Notice that as K_{24} increases beyond $2K_2$, the free energy decreases continuously

from 0, thereby confirming that the ET configuration as a ground state is preferred over the uniform configuration whenever it can exist; $K_{24} = 2K_2$ marks a second-order phase transition line. The key to this energetic stabilization is the saddle-splay term:

$$\frac{F_{24}}{\pi L} = -K_{24} \sin^2 \beta_1. \quad (6)$$

As noted in Ref. [34], in which the authors used an opposite surface normal convention, F_{24} couples the nematic director to the surface curvature tensor and favors alignment in the direction of highest curvature for $K_{24} > 0$. In our case, this is the azimuthal direction along the circumference of the capillary. Thus, the saddle-splay free energy stabilizes the ET configuration despite introducing bulk director distortion. We have also verified that both the ET and the deformation-free solutions are stable whenever they are preferred ($K_{24} > 2K_2$ and $K_{24} < 2K_2$, respectively); that is, their stability matrices have positive eigenvalues (see the supplemental material) [47].

Our experimental investigations used nematic SSY, a LCLC with relatively low twist modulus $K_2/K_3 \approx 0.1$ [16]. Briefly, five SSY samples were loaded into five different capillary tubes with diameters $100 \mu\text{m} \pm 10\%$, from VitroCom (CV1017-100). The sealed samples were illuminated between cross-polarizers by 10 nm band-pass-filtered 660 nm LED light at high (160 \times) magnification, enabling a small depth of field and high spatial resolution imaging. Images were captured by a Uniq UP680-CL video camera, and a piezo-objective positioner was moved to image focal planes within the samples in 1 μm intervals.

The capillaries without surface treatment were loaded with SSY and sealed to prevent evaporation. A critical experimental question for any saddle-splay study concerns the possible structure of cylindrical interfaces that would induce a preferred anchoring direction. Toward that end, we examined the inner capillary surfaces using atomic force microscopy (AFM) and scanning electron microscopy (SEM), and we compared the inner capillary surfaces to rubbed glass; the capillaries had no discernible grooved structures as on the rubbed glass. Since SSY is known to exhibit natural planar anchoring on smooth glass surfaces [29], our observations of the capillary surface strongly suggest that degenerate planar boundary conditions are present on the inner surfaces of the cylinders, and any anisotropic Rapini-Papoular-type anchoring effect would be small [22,38,47]. We also considered alignment caused by flow during capillary filling. Loading capillaries with the LCLC in either the nematic or the isotropic phase resulted in the same type of director configurations. Further, since the filling flow is nearly perpendicular to the final alignment found at the capillary surface, flow alignment appears unlikely. Finally, we considered the possibility that a layer of molecules adsorbed to the capillary surface sets an easy access at the capillary surface during or shortly after filling. We exclude this possibility by cycling the filled capillary between nematic and isotropic phase and observing that the director at the capillary surface retains no memory from cycle to cycle [47].

We measure the director angle, $\beta(r)$, directly by observing a flickering speckle pattern and its direction in the LC. The pattern originates from director field temporal fluctuations and accompanying fluctuations in the ordinary and extraordinary

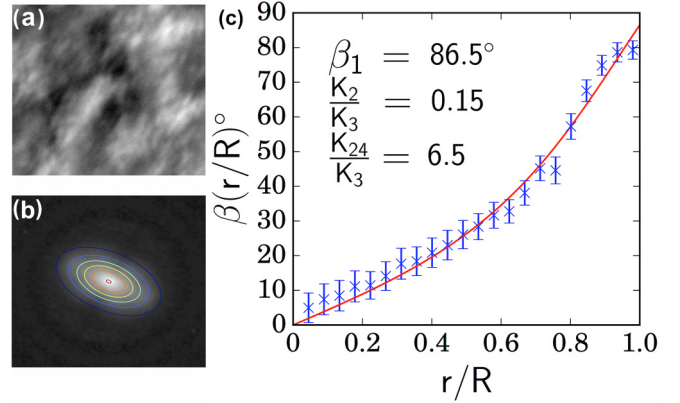


FIG. 3. (Color online) Representative flickering measurements of 30% wt./wt. SSY in a $90.6 \mu\text{m}$ capillary at 25°C . (a) Single frame from a movie cropped to a $20 \mu\text{m}$ square and after background subtraction (see main text). (b) Averaged FFT of a movie containing many images of fluctuations and a contour plot of a 2D Gaussian fit to the averaged FFT. The long axis of the fit is perpendicular to the dominant fluctuation direction and yields a measurement of β for the image slice. (c) Fit of Eq. (4) to $\beta(r)$ obtained by fluctuation measurements along the capillary radius. Error bars are the standard deviations in degrees of the angle found for the 2D Gaussian fits as in (b). A nonlinear least-squares fit of the parameters K_2/K_3 and K_{24}/K_3 gives estimates of the elastic constant ratios (6.5 and 0.15, respectively) for the sample. Across all measurements, the average $K_{24}/K_3 = 6.6$ and has a bounding interval [3.8,9.4].

refractive indices that cause scattering [25]. These types of fluctuations of the director field have been exploited previously to measure the viscoelastic ratios of liquid crystals [10–12]. Our work follows Ref. [11], which proposed using videos of LC flickering to discern local orientation of the director field [47]. Flickering shape and direction depend on the local director field configuration and LC viscoelastic anisotropy.

The experimentally measured $\beta(r)$ for one of the five LCLC samples studied is shown in Fig. 3(c). It is well fitted by the calculated expression [Eq. (4)], and the fitting provides experimental values for ratios of the twist-to-bend and saddle-splay-to-bend elastic constants. The twist-to-bend ratio is in close agreement with prior measurements [16]. Since $K_{24}/\sqrt{K_3 K_2} \sim \tan(\beta_1)$ when $K_{24} \gg K_2$, the fit values become increasingly sensitive to experimental uncertainties as $\beta_1 \rightarrow \pi/2$. For example, the fit value of K_{24}/K_3 is sensitive to the uncertainty of the measured size of the capillary radius, R [47]. For the data in Fig. 3(c), the capillary was measured to have a diameter of $90.6 \mu\text{m}$ to within $\approx \pm 0.4 \mu\text{m}$. This relatively small uncertainty, however, leads to the large uncertainty we give for our estimate of K_{24}/K_3 , i.e., K_{24}/K_3 has a mean value averaged across experiments of 6.6 with a bounding interval [3.8,9.4]. By contrast, K_2/K_3 is a stiff parameter in the fit; it has a mean value averaged across experiments of 0.12 and a standard deviation $\sigma_{K_2/K_3} = 0.04$ [47].

We also observed hedgehog defects associated with the ET configuration. In long capillaries, we typically observed ET domains of opposite-handedness separated by chiral point defects. These defects were qualitatively proposed in Ref. [39]. We observed annihilation of neighboring defects,

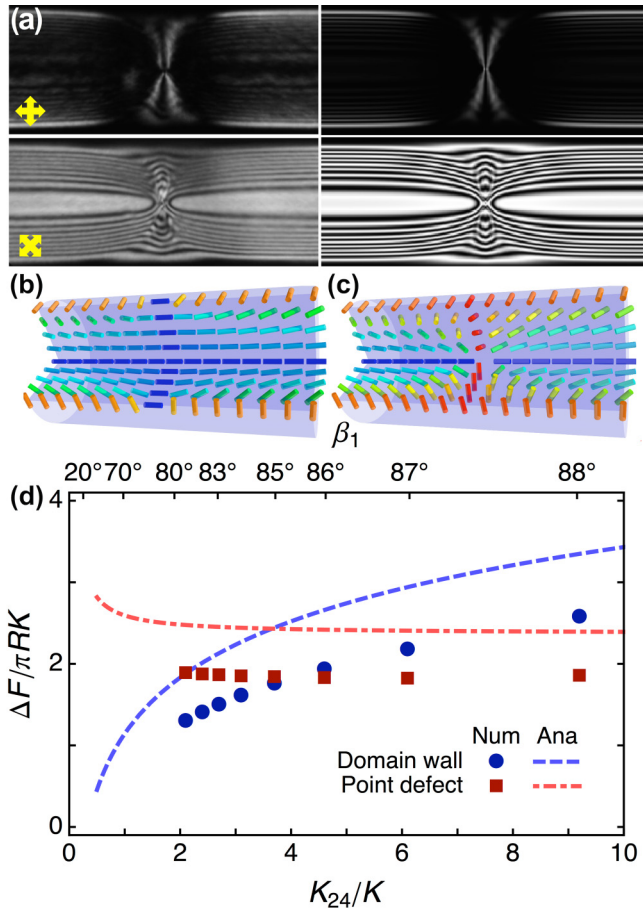


FIG. 4. (Color online) (a) Left: cross-polarized quasimonochromatic optical images of singular point defects bordering ET regions of opposite handedness in a $90 \mu\text{m}$ capillary. Yellow arrows indicate the polarizer pass axis directions. Right: images reconstructed using Jones matrix calculations from numerically computed director fields of defects. (b) A 3D cutaway view of a capillary with opposite-handedness ET regions separated by a wall defect. (c) A 3D cutaway view of a capillary with opposite-handedness ET regions separated by a point defect as imaged and simulated in (a). In both (b) and (c), the director field represents an LC with $K_2/K = 0.1$ and $K_{24}/K = 4.6$, where $K_1 = K_3 \equiv K$ and the color scale is the same as Fig. 1(b). (d) Energies of the point and domain-wall defects relative to the ET energy as a function of either K_{24}/K or equivalently β_1 , with $K_2/K = 0.1$. Points indicate numerical calculations and lines indicate analytical approximations [47]; the latter have higher energy than the former but demonstrate similar qualitative behaviors.

indicating that they carry opposite topological charge [47]. The presence of nematic director singularities is apparent in Fig. 4(a); bright-field microscopy [47] reveals dark spots from scattered light along the center of the capillary. Once found, we image the point defect under crossed-polarizers with the same illumination as described above. We compare these experimental textures with those simulated numerically using Jones matrices [47]. The comparison requires a test director configuration, which we calculate using Eqs. (1) and (2). For configurations in the presence of defects, however, the director depends on both r and z ; the boundary conditions at $z \rightarrow \pm\infty$ bring the director configuration back to ET configurations

with opposite-handedness. To arrive at an optimized guess, we solve the Euler-Lagrange equations numerically with a relaxational technique [47]. The configurations that emerge are very similar to what one gets if one takes the standard radial and hyperbolic hedgehogs and simply rotates all directors by $\pi/2$ about the z axis [47]. This simple operation, which is guaranteed to preserve hedgehog charge, automatically produces opposite chirality on opposite sides along z of the hedgehog defect regardless of the sign (± 1) of its charge. The topological charges of successive hedgehogs necessarily alternate in sign [47]. Using $K_1 = K_3 \equiv K$, $K_2/K = 0.1$, and $K_{24}/K = 4.6$, numbers that are consistent with our measurements in the ET ground state, we observed remarkable agreement between experimental and theoretical textures [Fig. 4(a)].

In principle, smooth domain walls can also separate domains of opposite-handedness, in which the escaped-twist configuration continuously untwists from one domain to the wall midplane and then continuously retwists with opposite-handedness into the other domain [see Fig. 4(b)]. In this case, throughout the midplane, the director would align along the capillary axis. However, in SSY, we have never experimentally observed such a domain-wall structure. Defect energetics provide an explanation for this observation, which has an interesting consequence. Again, we numerically calculate the configurations of both domain walls and point defects to obtain their energies [47]. For these calculations, we fix $K_2/K = 0.1$ in accordance with [16] and our fluctuation experiments, and we allow K_{24} to vary. As shown in Fig. 4(d), point defects (domain walls) have lower energy than domain walls (point defects) for $K_{24}/K \gtrsim 4$ ($K_{24}/K \lesssim 4$). Using $K_3 = K = 6.5 \text{ pN}$ from [16] and $R = 50 \mu\text{m}$, a typical dimensionless energy difference of $\Delta F / \pi R K = 0.1$ corresponds to $\Delta F = 2.5 \times 10^4 k_B T$, where $T = 298 \text{ K}$ is the experimental temperature. If K_{24} is greater than the crossover value $\approx 4K$, then, according to theory, one should not expect to observe smooth domain walls. Thus, both our observations of defects (or lack thereof) and our energy analysis set 4 as an approximate lower bound for K_{24}/K , in agreement with our fluctuation-measured value of $K_{24}/K = 6.6$ [3.8,9.4].

In summary, we have completed an experimental and theoretical study of a lyotropic chromonic liquid crystal, Sunset Yellow, in its nematic phase and confined in a hollow cylinder with degenerate planar boundary conditions. The escaped-twist configurations found to form in the bulk require a large saddle-splay modulus, which we have measured. We also observed point defects in this system whose existence (compared to the absence of smooth domain walls) provides independent confirmation of K_{24} . In the future, it will be interesting to study and manipulate these chiral configurations and investigate their formation from the isotropic phase.

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J.J., L.K., and Z.S.D. contributed equally to this work.

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- [48] A curvature-dependent anchoring energy, $F_w = \frac{w}{2} \int d^2S \mathbf{n} \cdot \mathbf{L} \cdot \mathbf{n}$, is allowed by symmetry and could arise from interactions between LC molecules/mesogens and the confining surface; here w is the anchoring strength, \mathbf{L} is the surface curvature tensor, and d^2S is the magnitude of the surface area element. In principle, changes in surface chemistry on the container surface can vary the magnitude and/or sign of w . If $|F_w|$ is not small, then its explicit separation from saddle-splay contributions will require experiments using the same LC but in cylinders with different surface chemistry.
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